

# Implementation of Perturb & Observe and Fuzzy Logic Control MPPT of PV System Using SEPIC Converter

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## Abstract

This paper presents the controller design of the PV system implemented with the single-ended primary inductance converter (SEPIC). The objective is to improve the efficiency of a standalone solar energy system consisting of a photovoltaic (PV) panel and a DC/DC SEPIC converter connected to a load. In this study, simulation of Perturb & Observe (P&O) and Fuzzy Logic (FL) Maximum Power Point Tracking (MPPT) are used in photovoltaic system with a direct control method are presented. In this control system, no proportional or integral control loop exists and a P&O algorithm and an adaptive FL controller generate the control. The designed and integrated system is a contribution of different aspects which includes simulation, design and programming. MATLAB/Simulink software is utilized for simulation. The obtained experimental results show the functionality and feasibility of the proposed controller.

**Keywords:** SEPIC Converter, Perturb & Observe (P&O,) Fuzzy Logic Controller (FLC), Maximum Power Point Tracking (MPPT), Photovoltaic (PV).

## 1. Introduction

Significant progress has been made over the last few years in the research and development of renewable energy systems such as wind, sea wave and solar energy systems. Among these resources, solar energy is considered nowadays as one of the most reliable, daily available, and environment friendly renewable energy source [1], [2]. However, solar energy systems generally suffer from their low efficiencies and high costs [3]. In order to overcome these drawbacks, maximum power should be extracted from the PV panel using different MPPT techniques to optimize the efficiency of overall PV system. MPPT is a real-time control scheme applied to the PV power converter in order to extract the maximum power possible from the PV panel. For a fixed load, the equivalent resistance seen by the panel can be adjusted by changing the power converter duty cycle [4]. The Fuzzy Logic (FL) and the Perturb and Observe (P&O) are most known and commercially used techniques [5]-[8]. Other modified methods have been also reported to improve the performance of these techniques.

Two common choices of DC-DC switching converters for photovoltaic system are SEPIC and buck-boost converters. An implementation of the SEPIC converters for MPPT in [1] shows a satisfactory performance. Although a buck-boost converter is simpler, its output voltage is inverted. Combining a buck converter with a boost converter eliminates the inversion, but adds complexity. So, when non-inverted output voltage is required, a SEPIC would be a better choice as observed in [2].

### 1.1 Overview of the Project

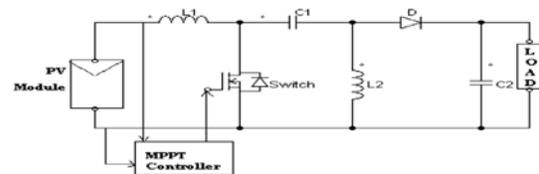


Fig. 1 Proposed converter with MPPT controller.

Fig.1 shows the closed loop analysis of SEPIC converter with PV module and MPPT algorithm controller. The P&O method is commonly used because of its simplicity and ease of implementation [5]-[8]. Furthermore, P&O (with a small step size) in nominal conditions can have MPPT efficiencies mostly the same like other complex techniques, and still easier implementation [6]. However, the drawback of this technique is that the operating point of the PV array oscillates around the MPP. Therefore, the power loss may increase. Furthermore, when the sun direction changes rapidly, the P&O method probably fails to track the MPP. Another possible disadvantage is that the MPPT may not be able to locate the MPP as the amount of sunlight decreases, because the PV curve flattens out [5]. In order to overcome these drawbacks and improve the P&O response, many techniques are suggested and investigated in the literature such as, the introduction of three-point weight comparison P&O algorithm [7] and the use of modified adaptive techniques [8]. This paper proposes a new fuzzy based

MPPT technique to adaptively change voltage step-size depending on the PV system operating point and the old step-size. The proposed control scheme achieves stable operation in the entire region of the PV panel and eliminates therefore the resulting oscillations around the maximum power operating point.

## 2. PV System Model

The proposed standalone photovoltaic (PV) system consists of three main blocks: PV panel, power converter, and MPPT controller. The following sections will describe the modeling of the PV panel and power converter.

### 2.1 PV Panel Model

The PV model represents the solar cell in its simplest form as a PN junction followed by a series resistance as shown in Fig. 2 [10]. The PV system equivalent circuit is described by the following equations:

$$V_{cell} = V_D - I_{cell}R_s \tag{1}$$

$$I_{cell} = I_{ph} - I_D = I_{ph} - I_o (e^{K_{PV}(V_{panel} + I_{cell}R_s)} - 1) \tag{2}$$

Where  $V_{cell}$  is the PV cell terminal voltage,  $V_D$  is the diode voltage,  $I_{cell}$  is the PV cell terminal current,  $I_D$  is the diode current.  $K_{pv} = \frac{q}{pKT}$ ,  $q = 1.6 \times 10^{-19}$  C (electron charge),  $K = 1.3805 \times 10^{-23}$  J/K (Boltzmann's constant),  $T$  is the cell temperature, and  $p=1.3$  is the ideal p-n junction characteristic factor for monocrystalline solar cells [10].  $I_o$  is the saturation current in diode reverse-biased direction and  $R_s$  is the panel series resistance:

$$I_o = I_{rr} \left( \frac{T}{T_r} \right)^3 e^{\left( \frac{qV_g}{pK} \left( \frac{1}{T_r} - \frac{1}{T} \right) \right)} \tag{3}$$

Where  $I_{rr}$  is the reverse saturation current at the reference temperature  $T_r$ .  $V_g$  is the band-gap voltage of the semiconductor making up the cell, which equals 1.12 eV for monocrystalline Si cells, and  $I_{ph}$  is the Photocurrent

$$I_{ph} = (I_{sc} + K_I(T - T_r)) \frac{\lambda}{100} \tag{4}$$

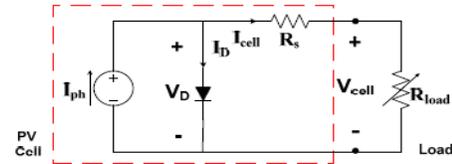


Fig. 2 PV system circuit model.

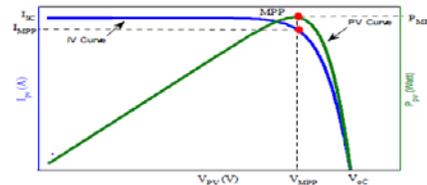


Fig. 3 PV panel characteristics.

$I_{sc}$  is the short-circuit cell current at reference temperature and insolation,  $K_I$  in (mA/K) is the short-circuit current temperature coefficient,  $\lambda$  is the insolation in (MW/cm<sup>2</sup>), and  $I_o$  is the saturation current in diode reverse-biased direction.

The panel IV and PV characteristics curves are obtained by plotting the PV current and PV power as a function of the PV voltage as shown in Fig. 3.[12] This figure illustrates also the location of three important points on the PV panel characteristics: the short-circuit current  $I_{sc}$ , the open-circuit voltage  $V_{oc}$ , and the maximum power point  $V_{MPP}$ ,  $I_{MPP}$ ,  $P_{MPP}$ .

### 2.2 Power Converter

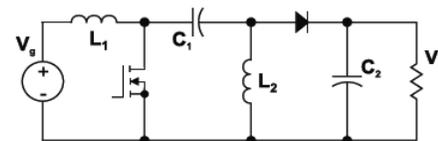


Fig. 4 SEPIC converter

The buck–boost feature of the SEPIC widens the applicable PV voltage and thus increases the adopted PV module flexibility and still has the merits of non-inverting polarity, easy-to drive switch, and low input-current pulsating for high-precise MPPT that makes its integral characteristics suitable for the low-power PV charger system[19]. One converter that provides the needed input-to-output gain is the Sepic (single- ended primary inductor converter) converter. A Sepic converter is shown in Fig. 4. It has become popular in recent years in battery-powered systems that must step up or down depending upon the charge level of the battery. Fig. 5 shows the circuit when the power switch is turned on. The first inductor, L1, is charged from the input voltage source during this time. The second inductor takes energy from the first capacitor, and the output capacitor is left to provide the load current. The fact that both L1 and L2 are disconnected from the load when the switch is on leads to complex control characteristics.

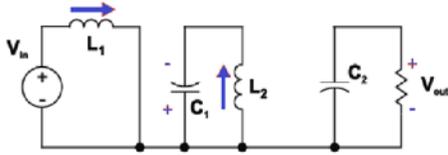


Fig. 5 Mode-1 of SEPIC converter when switch is ON

When the power switch is turned off, the first inductor charges the capacitor C1 and also provides current to the load, as shown in Fig. 6. The second inductor is also connected to the load during this time.

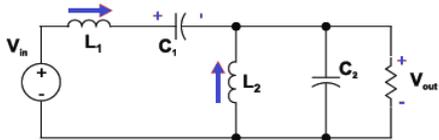


Fig. 6 Mode-2 of SEPIC converter when switch is OFF

### 3. Maximum Power Point Tracking

For maximizing the PV conversion efficiency, the incoming sun energy must be converted to electricity with the highest efficiency, accomplished when the photovoltaic module operates on the maximum power point. Nevertheless, since this operating point is strongly affected by the solar radiation and temperature levels [18]. Thus, in order to dynamically set the MPP as operation point for a wide range of solar radiation and temperature, specific circuits, known at the literature by Maximum Power Point Trackers (MPPT), are employed. There are many MPP algorithms, here the implementation of two such algorithms namely Perturb & Observe (P&O) and Fuzzy Logic (FL) controllers are used in the simulation.

#### 3.1 Perturb & Observe

Perturb and Observe (P&O) is one of the most diffused MPPT algorithms, whose tracking response is independent on the environmental conditions, however, its implementation requires a voltage and a current sensor, increasing the cost and complexity.

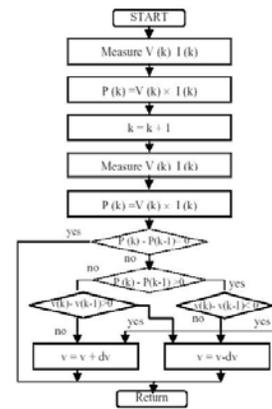


Fig. 8 Flowchart of Perturb & Observe method

#### 3.2 Fuzzy Logic Control

Fuzzy logic control is a new addition to control theory. Its design philosophy deviates from all the previous methods by accommodating expert knowledge in controller design. The fuzzy control does not need an accurate mathematical model of a plant. Therefore, it is applicable to a process where the plant model is unknown or ill defined. To implement the FL in a problem, different steps of this algorithm must be taken which are as follows.

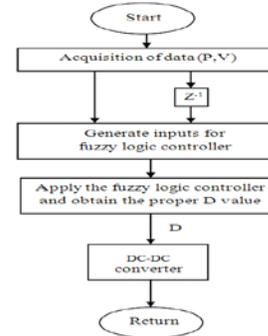


Fig. 6 Flowchart of Fuzzy Logic Control

##### 3.2.1 Fuzzification

The input defined in Equations (5) and (6) need to be fuzzified by some membership functions. For each input value, the respective membership function returns a value of  $\mu$ . The max-min method was applied to extract the  $\mu$  from the triangle type membership function.

$$e(t) = \frac{\Delta P(t)}{\Delta V(t)} = \frac{\Delta P(t) - \Delta P(t-1)}{\Delta V(t) - \Delta V(t-1)} \quad (5)$$

$$\Delta e(t) = e(t) - e(t-1) \tag{6}$$

### 3.2.2 Inference Diagram

A rule base must be applied to the obtained membership function according to Mamdani. The rule table is designed and shown below in Table 1.

### 3.2.3 Defuzzification

For the Defuzzification, the centroid method is applied to return a proper value for the duty cycle variation ( $\Delta D$ ). The defuzzified output value of the FLC must be added to a reference value of duty cycle which is considered equal to the duty cycle for the current study [10]. The result is the optimum value of D that has to be sent to the SEPIC converter as a control signal.

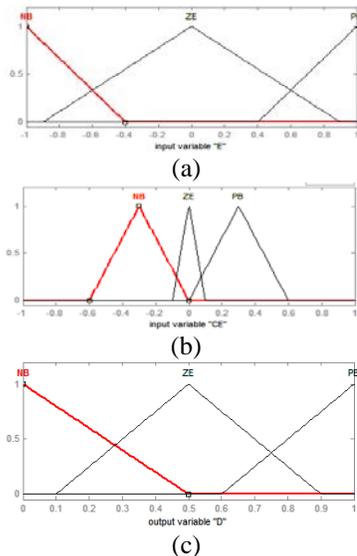


Fig. 9 Membership function of (a) input e, (b) input  $\Delta e$  and (c) output  $\Delta D$

Figure 9 as shown above depicts the membership functions for inputs  $e$  and  $\Delta e$  and output  $\Delta D$  which is the variation needs to be applied to the current D value.

Table 1: Rule Table

$e/\Delta e$	<b>NB</b>	<b>ZE</b>	<b>PB</b>
<b>NB</b>	PB	PB	PB
<b>ZE</b>	PB	PB	PB
<b>PB</b>	PB	PB	PB

## 4. Simulink Design of Proposed System

Simulation is a process in which the circuit works and verifies the output values. Figure 10 and figure 11 show the P&O and FL algorithm controller respectively. Here both algorithms output voltage waveform are compared to show which controller is best to provide an efficient system.

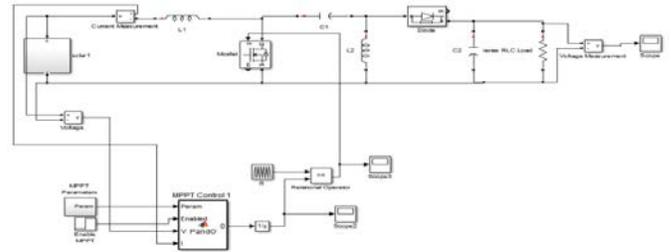


Fig. 10 Simulink model of closed loop system with P&O algorithm controller

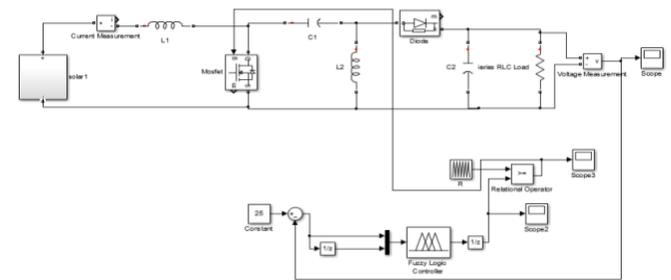


Fig. 11 Simulink model of closed loop system with Fuzzy Logic algorithm controller

The parameters of the PV panel and the SEPIC converter are shown below in the Table 2 and Table 3.

Table 2: PV panel parameters

$P_{max}$	$V_{max}$	$I_{max}$	$V_{oc}$	$I_{sc}$
10W	17V	0.588A	21.6V	0.659A

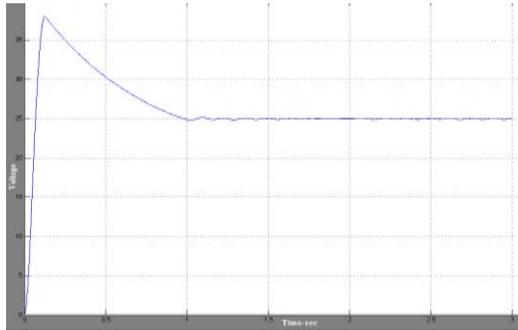
Table 3: SEPIC converter parameters

$V_{in}$	$V_{out}$	Switching frequency	$L_1$	$L_2$	$C_1$	$C_2$
32V	24V	500Hz	6.4mH	32mH	62.5 $\mu$ f	41.66mf

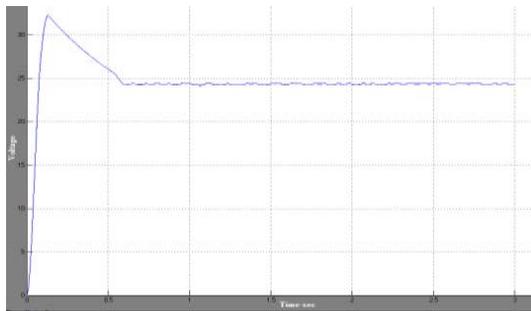
## 5. Simulation Results

The PV module is modeled in MATLAB/SIMULINK with the assumption that the PV module has constant temperature of 25°C, at an Insolation level of 1000W/m<sup>2</sup>. A pure resistive load is connected to the PV module through the SEPIC converter. The performance of the proposed technique has been examined

for fixed solar radiance at  $1000\text{W/m}^2$  in P&O method and variable irradiance in FL method.



(a)



(b)

Fig. 12 P&O and Fuzzy Logic, responses for standard conditions of temperature  $25\text{ }^\circ\text{C}$  for irradiation  $1000\text{W/m}^2$

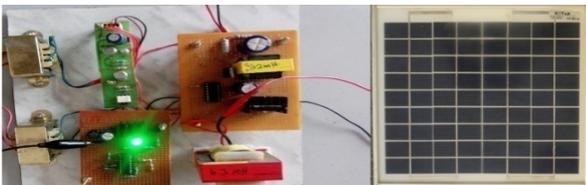


Fig. 13 PV system with experimental SEPIC converter and a driver circuit

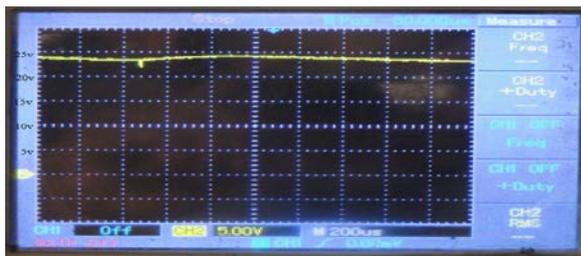


Fig. 14 Output voltage shown in CRO

Fig.12 (a) & (b) shows the results of PV operating voltage of the triangular membership functions. From this figure, it is observed that the fuzzy can track the maximum power point better than Perturb & Observe method. Hence from the investigation, it is clear that the PV power which is controlled by the proposed fuzzy controller is more stable than the conventional MPPT techniques. A photograph of the experimental converter is shown in Fig. 13, and the response to

an input voltage, the output voltage is shown in Fig. 14. From the data given in Table 4, it is observed that the fuzzy can track the maximum efficiency compared to the conventional P&O MPPT techniques.

Table 4: Comparison of MPPT technique

MPPT methods	Output voltage	Peak overshoot	Settling time
P&O	25v	38v	1sec
FLC	24v	33v	0.6sec

## 6. Conclusions

This paper has presented an intelligent MPPT control strategy for the PV system using fuzzy logic controller. The maximum power point tracking technique was simulated using MATLAB/Simulink. The proposed fuzzy logic based MPPT technique can track the maximum power point faster compared to the P&O based mppt technique. It has the capability of reducing the voltage fluctuation after MPP has been recognized. The simulation results show the efficiency of the fuzzy logic controller in maintaining the stable maximum power point.

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