

# Sensorless Vector Control Of Permanent Magnet Synchronous Motor Based On Current Sampling

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**Abstract:** Sensorless vector control strategy of permanent magnet synchronous motor (PMSM) based on IRMCF341341 is introduced, and rotor position detection based on a low cost of current sampling strategy is presented. No position system simulation model and system software and hardware design are built. The test results show that the control strategy is feasible and practical in the application of permanent magnet synchronous motor.

**Keywords:** PMSM; no position sensor; vector control ;IRMCF341; current sampling;

## 0 Introduction

Permanent magnet synchronous motor don't need exciting current, operating efficiency and power destiny are both very high, however its high-performance control needs accurate rotor position and rate signal to achieve flux-oriented control. In motion control system of traditional permanent magnet synchronous motor, usually we use photoelectric coding disk or resolver to sampling rotor position and rotor rate. However, these sensor raises the cost of system control, and reduced the reliability of the system. Therefore, it becomes more and more popular to call off these devices to improve the reliability of the system.

## 1 Vector control of permanent magnet synchronous motor

This article uses vector control which based on  $i_d=0$ , for permanent magnet synchronous motor we use the control mode of  $i_d=0$ , we can linearly control torque of the motor by control the size of quadrature axis currents.

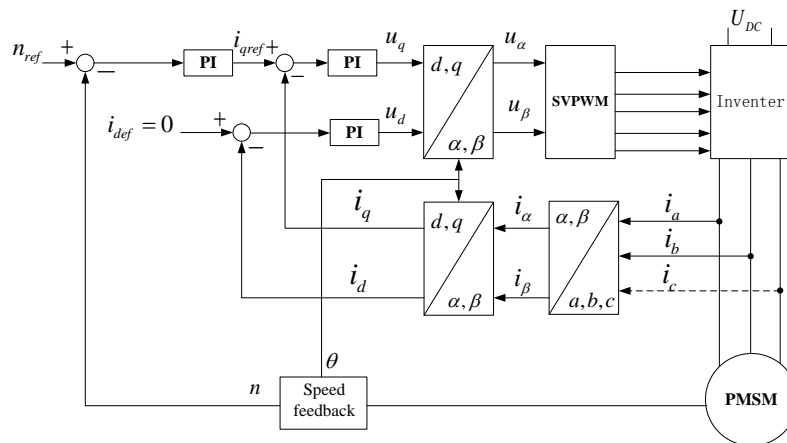


Fig.1 Vector control block diagram of permanent magnet synchronous motor based on  $i_d = 0$

Firstly, the rotor position and speed acquisition unit system speed, the speed difference between the output and the speed of set by PI controller is used as the reference value of the torque current component, excitation current component of the reference value of is set to 0, the motor stator windings of three-phase current, by Clark transform and after the Park transform get

actual torque component of current and excitation current component, two components were set by PI and the difference between the regulator output voltage under the rotating coordinate component and, two components by Park inverse transform in two-phase static coordinates and voltage component, The two component is modulated by the SVPWM module generates six PWM signals to the three-phase inverter, the inverter control motor speed and torque.

## 2 The simulation study of sensorless

### 2.1 Strategy of sampling of low-cost current

At present, most of permanent magnet synchronous motor driver generally use at least two hall current sensor to sampling the phase current of the motor. Obviously this simulation raised the cost and complexity level. Therefore we need a kind of simulation of current sampling which is low-cost and for the best it has only one current sampling unit. One way which is grown is to using current and PWM signal to rebuild the project of phase current of the motor. This system is built with this low-cost current sampling simulation.

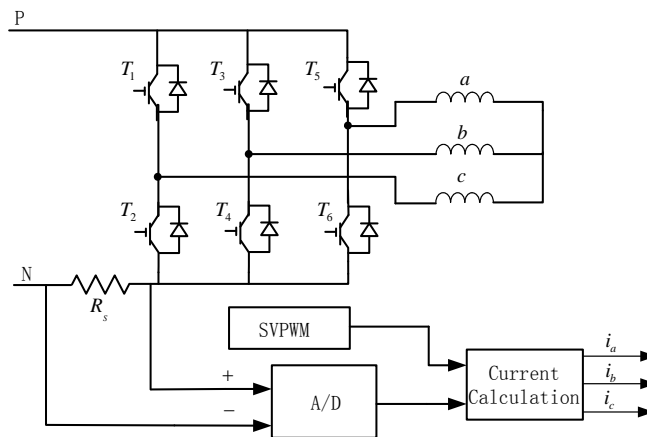


Fig.2 System structure based on bus current sampling

$R_s$  is sampling resistor in negative DC side voltage of the A/D converter, direct acquisition sampling resistor value. Combined with the PWM switch vector information of the current draw phase current value, the following will analyze the relationship between the bus current and PWM vector.

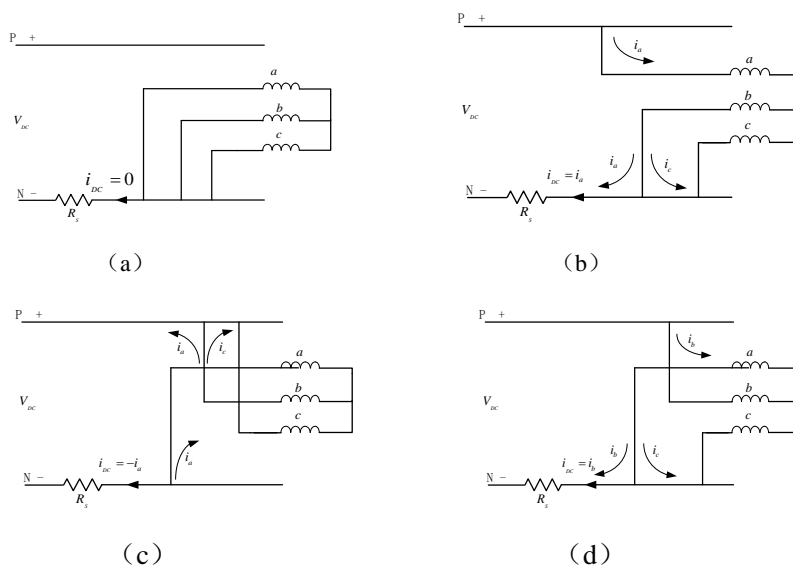


Fig.3 DC bus current under different switching vectors

As shown in Figure 4 there are two non-zero switching vectors in each PWM period. There is two different phase current in each PWM period. DC bus can get another phase current value through a simple addition and subtraction. Thus the motor phase current sampling method is feasible in order to obtain better effect. The sampling, is proposed to avoid the influence of sampling switch brings the switch in the middle of vector function time, as long as the and time sampling can be obtained respectively and calculated, can also choose in the current set up stable immediately after sampling. There are also researchers proposed Due to the phase current, frequency of the motor is much lower than the switching frequency of PWM, so it can be considered that in a PWM cycle phase current is constant, so it can be in the first half of the PWM cycle in the moment for the first time the current sampling, and wait until the second half cycle time second electric current sampling. The advantage of this is that between widening A/D converter two conversion interval, greatly reduce the performance requirements of the A/D converter.

Tab.1 Table of the relationship between switching state and sampling current

Switch State	000	100	110	010	011	001	101	111
Sampling Current	$0$	$i_a$	$-i_c$	$i_b$	$-i_a$	$i_c$	$-i_b$	$0$
Sector	$V_0$	$V_1$	$V_2$	$V_3$	$V_4$	$V_5$	$V_6$	$V_7$

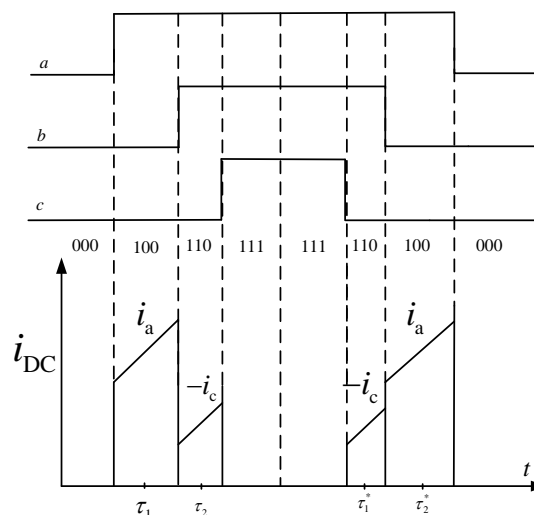


Fig.4 The relationship between the switching state of a PWM cycle and bus current in an ideal condition

## 2.2 Rotor position decision modeling and simulation

Low cost current sampling method presented above, the three-phase current through the sampling resistor negative bus can obtain the motor, this section through the simulation modeling to determine the rotor position of permanent magnet synchronous motor.

Permanent magnet motor normal operation current in the three-phase winding is the same frequency with the phase difference of 120 degree sine wave, strategy we have to obtain the current in the three-phase winding from the current day sampling to obtain the rotor position information as follows from the modeling and Simulation of three-phase current.

In a circuit as an example, the V3 phase current windings, the design is used in the input and output of the comparator four, when the V3 is in the upper half sine ( $> 0$ ) comparator output is 0, when the V3 is in the lower half sine ( $< 0$ ) the output of the comparator for VCC. Three similarly, the output of wave signal is the same frequency and the phase difference of 120 degree square.

Fig.5 Rotor position simulation of a phase current

Figure 6 is a comparison of two input output current, input signal frequency the same phase difference of 120 degrees, the output frequency is the same with the phase difference of 120 degree square wave signal.

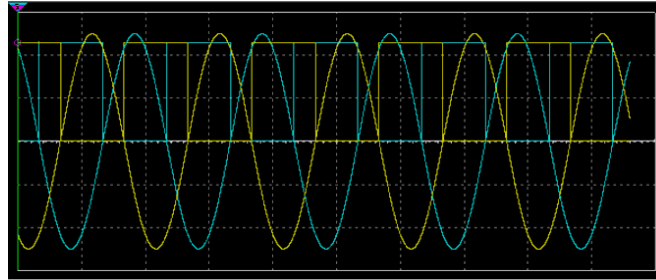


Fig.6 Two input - output contrast diagram

Figure 7 is a three-phase square wave output signal, a record high level time is 1, the low level of 0, in a power cycle three-phase winding signal can be expressed by the following figure.

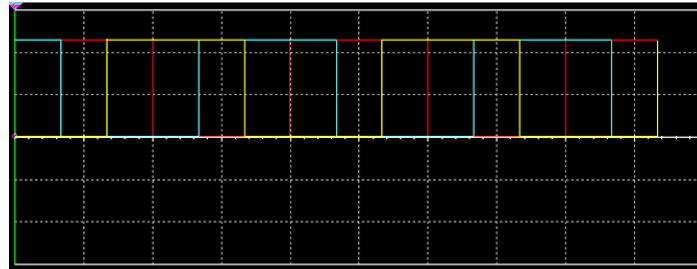


Fig.7 Three phase square wave output

Remember a moment of high level is 1, the low level of 0, according to figure 7 can wait until a period of electric rotor position of the sector Table 2 contact sections, namely through the sampling resistor negative bus can get to the three-phase current information, in accordance with this section through the three-phase current to obtain the rotor position and sectors, so as to achieve control of the motor.

Tab.2 Rotor position sector table

A	B	C	Sector
1	0	0	$V_1$
1	1	0	$V_2$
0	1	0	$V_3$
0	1	1	$V_4$
0	0	1	$V_5$
1	0	1	$V_6$

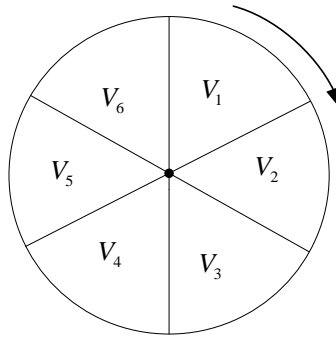


Fig.8 Rotor position sector

### 2.3 Without position sensor simulation and modeling

According to the permanent magnet synchronous motor rotor position determination method and vector control strategy, we first construct the simulation model of permanent magnet synchronous motor as  $i_d = 0$  position sensorless control of the double loop.

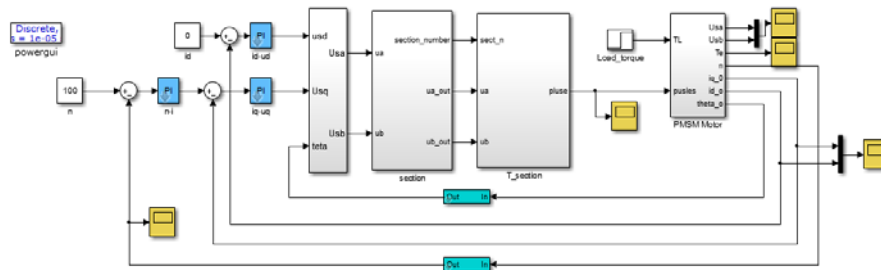


Fig.9 Vector control model of double closed loop permanent magnet synchronous motor

Figure 9 is a double closed loop of permanent magnet synchronous motor vector control simulation model, the inner loop adopts vector control strategy, the outer loop is the speed tracking.

The parameters of motor  $R = 1.11\Omega$ ,  $L_d = 16.6e-3H$ ,  $L_q = 16.45e-3H$ ,  $|\Psi_f| \approx 0.5072wb$  set the load torque for a given speed 2000, get the speed response waveform and phase voltage waveforms respectively. Figure 10 can be seen after the starting of the motor speed with speed setting quickly run to the 2000 system, fast response, small overshoot, good control performance.

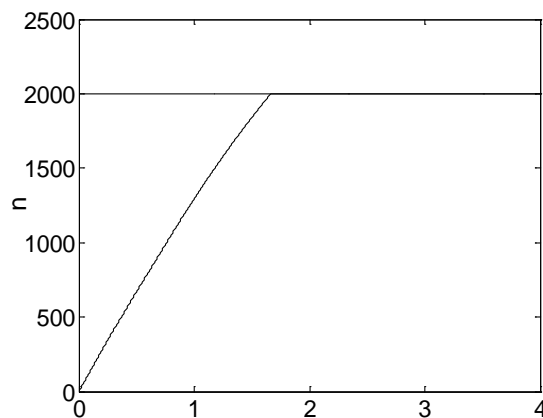


Fig.10 Speed response

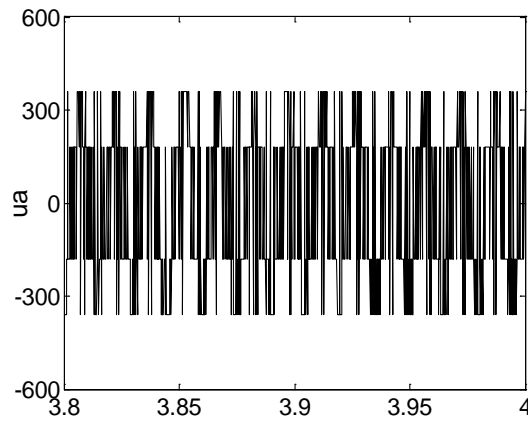


Fig.11 Phase voltage

### 3 The hardware and software system design

#### 3.1 Hardware design

##### 3.1.1 Power circuit

The design of the driving circuit with intelligent power module IPM, intelligent power module not only the switching device and the drive circuit are integrated together, and has integrated overcurrent, overheating and short circuit protection and fault detection circuit. The design of the IPM intelligent power module PS21A79 Mitsubishi, the maximum input voltage 600V, maximum output the current 75A, maximum switching frequency is 20KHz, can well meet the design requirements of control system.

##### 3.1.2 Power supply circuit

The system needs to provide the required power supply circuit to each chip, switching power supply control chip with high performance fixed frequency current mode UC2843BD1. controller of TI company

The main power supply circuit for 150~300V DC input, switch transformer output a 15V/500mA to provide 15V reference voltage for the power supply control chip, the power switch transformer output a 6V~7V/500mA three terminal regulator SPX1117-3.3 and SPX1117-1.8 in cascade output 3.3V/1A and 1.8V/ 1A respectively provide power supply for the IRMCF341.

##### 3.1.3 negative bus single resistor current sampling circuit

The current sampling precision and real-time largely determines the system's dynamic and static performance, current detection precision is to improve the system control precision, stability and rapidity of the important link, is to achieve the high performance of the closed-loop control system of key internal integrated. IRMCF341 12 AD 1.8V power supply, the input voltage range is 0~1.2V. The reference voltage for the MCE is 0.6V. The sampling circuit as shown in figure 12:

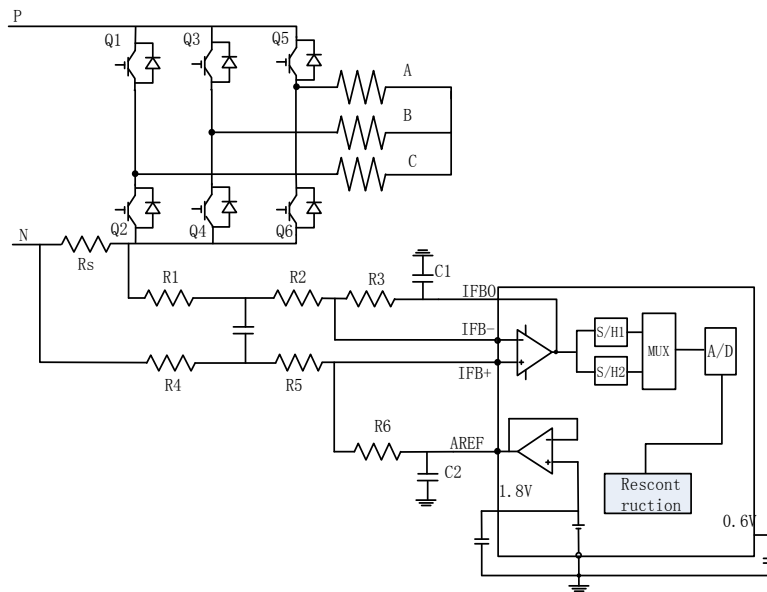


Fig.12 Single resistance current sampling circuit

$R_s$  is sampling resistance, this design selection  $R_s = 10m\Omega$ ,  $R_1 = R_4 = 1K$ ,  $R_2 = R_5 = 4K$ .

The current amplifier gain:

$$A = \frac{R_3}{R_1 + R_2} = \frac{10}{1 + 5.1} = 1.6393$$

So the 1A current can reflect the input terminal of the signal in AD:

$$10m\Omega \times 1.6393 = 16.38mV$$

The corresponding values for AD quantization:

$$16.39mV \times \frac{4096}{1200} = 56 \quad (\text{AD } 0-1.2V \text{ corresponding to } 0-4095)$$

However, due to the resistance error, gain error and other reasons, the current ratio is a bit error in figure C76 is part of high frequency oscillation signal filter sampling current, the general value of 47pF, the whole gain amplifier circuit can be neglected.

### 3.2 Software design

The system software is programmed by C, which is mainly composed of the main program and interrupt service subroutine, the main program complete hardware initialization, definition and initialization of variables within the inverter set and initialization state detection and program. Interrupt service subroutine includes PWM interrupt service subroutine and interrupt subroutine, over-voltage, over-current protection, drive protection, complete blockade pulse and alarm function. Then enter the open loop start program, set the timer T1 as the system clock, running into the closed loop. PWM interrupt current voltage detection, rotor position detection, speed estimation, speed loop and current loop PI control, Space vector modulation and PWM signal output. The program block diagram shown in Figure 13.

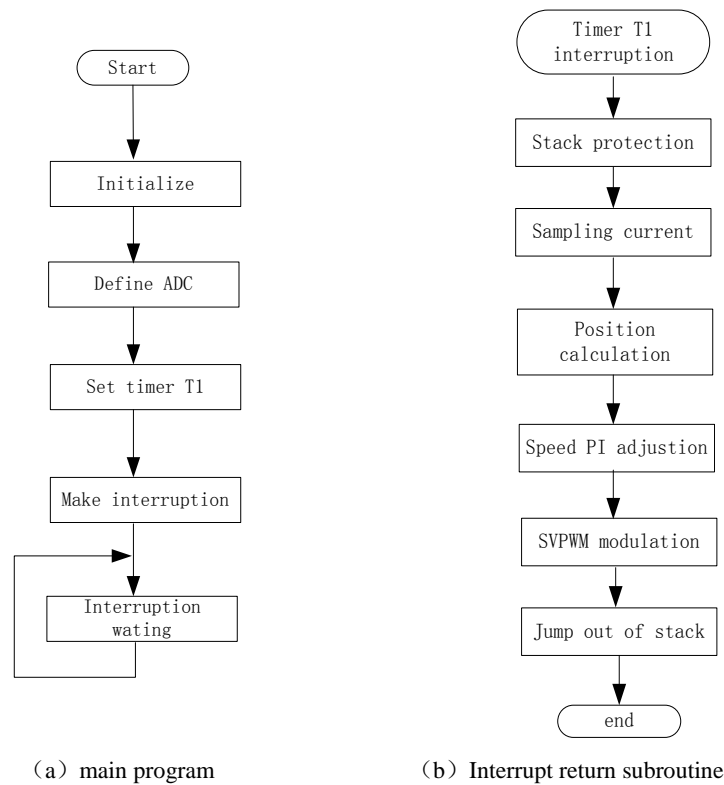


Fig.13 Block diagram

## 4 Experimental study

According to the requirements of the software and hardware design, this paper constructed IRMCF341 permanent magnet synchronous motor based on position sensorless vector control system.

Figure 14 is the starting of motor phase current waveform, Figure 15 is no-load speed of 2250rpm (Figure 4500 value corresponding to the 2250rpm), the phase current waveform and motor speed tracking waveform. The machine starts with four stages, one stage is Park rotor positioning stage, the phase current waveform by forcibly injected DC current is the rotor of the motor to reach the designated position and stops at the position, the sensorless FOC algorithm to know the exact position before the start of the rotor; the second stage is the open-loop acceleration stage, estimate the rotor angle using the motor model is simple; the third stage is the closed loop acceleration stage, transport speed To 500rpm (1000 value corresponding to the 500rpm loop) starting stage, motor speed up, speed up the voltage of the motor, the rotor angle of useful information extracted from the motor voltage and motor into the closed loop mode; the fourth stage is the stage of stable operation, the closed-loop operation of the motor to the setting speed, sustained and stable operation the phase current map in the open. There is a big wave ring stage, with no load, open loop switching point 500rpm and 2250rpm set the great speed difference between the cause.



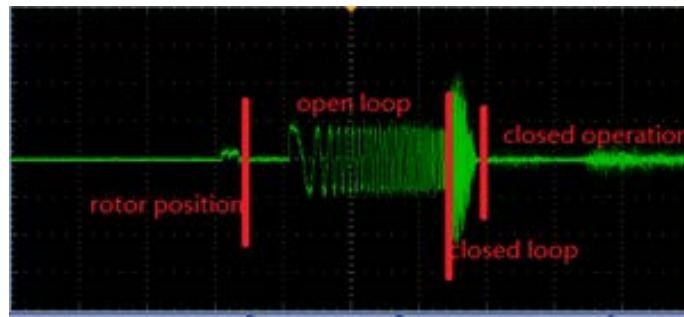


Fig.14 Motor starting phase current

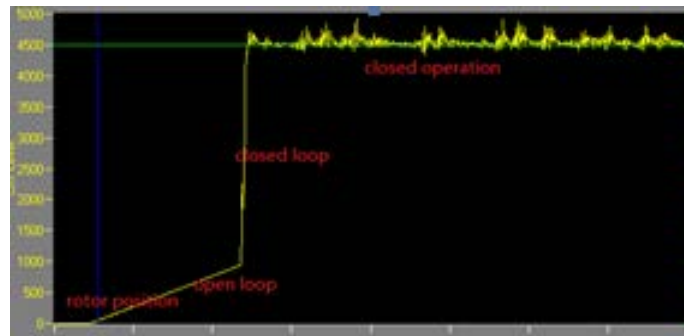


Fig.15 Motor start speed waveform

## 5 Conclusion

This paper presents sensorless control of permanent magnet synchronous motor based on IRMCF341 control chip and the sampling strategy and determine the position of the rotor current detection method based on a low cost current was set up. The position system simulation model and system hardware and software design, test results show that the control strategy can in the permanent magnet owns the feasibility and practicability of using synchronous motor.

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